IMPROVEMENT OF CLASSICAL EVOLUTIONARY PROGRAMMING USING STATE FEEDBACK CONTROLLER

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ABSTRACT. In evolutionary programming, each parent has two pieces of information: location and cost. The cost of parent specifies whether its location is suitable for breeding offspring or not. If the parent's cost is an acceptable value, producing offspring (or even steering other offspring) in the parent's area is advisable. This information is used in estimating the region of global minimum; then, using the state feedback controller, the offspring is steered to the optimal region. In the proposed method, the cost and coordination of parents have been used for breeding more elite individuals. Many (sixty-five) wellknown cost functions have been selected from different references to reveal the pros and cons of our algorithms. In the first stage, the proposed algorithm has been compared inside the EP family. This stage shows promising results for the proposed algorithm. In the second stage, comparison has been performed out of the EP frontiers in which algorithms are state-of-the-art in the optimization field, and are well known inside and outside of their own families. The statistic test has been performed among the algorithms. CPU time and its sensitivity to variable bounds, population and cost function dimensions have been studied. Finally, the proposed method is used in designing the nonlinear minimum variance controller for CSTR (Continuous Stirred-Tank Reactor) benchmark system. Keywords: Evolutionary programming, Weighted mean point, State feedback controller, Global optimization, CSTR benchmark system

1. Introduction. In the case of evolutionary computation, there are four historical paradigms which have served as the basis for many of the activities in the field: Genetic Algorithms (GA) (Holland and Harbor, 1975) [1], Genetic Programming (GP) (Koza, 1992) [2], Evolutionary Strategies (ES) (Recheuberg, 1973) [3] and Evolutionary Programming (EP) (Fogel et al., 1966) [4]. The basic differences between the paradigms lie in the nature of the representation schemes, reproduction operators and selection methods [5].

In conventional EAs, there is no feedback from the produced or cached information in deciding the coordinate of the new offspring. In addition, in conventional EAs, especially in EP, the region of each parent is the location for breeding the related offspring [6]; thus, the place and cost of other parents are not effective in deciding the coordinate of the offspring. However, the cost of parent specifies whether its location is suitable for breeding offspring or not. Using this information, an algorithm can enhance its performance.

In this paper, an improved version of CEP (Classic EP) is introduced in order to boost EP's performance in searching for the global minimum of multimodal cost functions. The

proposed method attempts to benefit from more information found in each iteration. If the parent's cost is acceptable among others, producing offspring near to its area and even steering other offspring toward that area is advisable. This approach enhances elitism in searching the cost plate.

The proposed algorithm is compared in and out of the evolutionary programming family. Inside the EP family, some well-known algorithms are selected for comparison. Outside the EP family, three groups of families are selected for comparison. Each family has one candidate for comparison. An attempt is made to select the algorithms that are highly capable and similar to the proposed method in methodology and style of searching the global minimum.

The organization of this paper is as follows. Section 2 presents a brief explanation on the background of algorithms. Section 3 introduces the basic ideas behind the Weighted Mean Classical Evolutionary Programming (WMCEP). Section 4 gives some details on test functions, and shows and compares simulation results. Section 5 includes statistic test of "Contrast Estimation of Median" among the algorithms. Section 6 tests sensitivity of CMA-ES (Covariance Matrix Adaptation Evolution Strategy) [7] and WMCEP methods on changes in parameters and compares the methods concerning CPU time. Section 7 presents an application of designing nonlinear minimum variance controller using WMCEP, and finally, Section 8 presents the conclusions and summarizes the simulation results.

2. Problem Statement and Preliminaries. The CEP can be implemented as follows

- [8] (This is the algorithm of EP as implemented in this paper.):
- 1) Generate the initial population of μ individuals and set k = 1. Each individual is taken as a pair of real valued vectors, (x_i, η_i) , $\forall i \in \{1, \ldots, \mu\}$, where x_i s are objective variables and η_i s are standard deviations for Gaussian mutations (also known as strategy parameters in self-adaptive evolutionary algorithms).
- 2) Evaluate the fitness score for each individual $(x_i, \eta_i), \forall i \in \{1, \ldots, \mu\}$ of the population based on the objective function $f(x_i)$.
- 3) Each parent $(x_i, \eta_i), i = 1, \dots, \mu$ creates a single offspring (x'_i, η'_i) by: $j = 1, \dots, n$
- 4)

$$x'_{i}(j) = x_{i}(j) + \eta_{i}(j)N_{j}(0,1)$$
(1)

$$\eta'_{i} = \eta_{i}(j) \exp(\tau' N(0, 1) + \tau N_{j}(0, 1))$$
(2)

where $x_i(j)$, $x'_i(j)$, $\eta_i(j)$ and $\eta'_i(j)$ denote the *j*th component of the vectors x_i , x'_i , η_i and η'_i , respectively. N(0,1) denotes a normally distributed one-dimensional random number with the mean of zero and standard deviation of one. $N_j(0,1)$ indicates that the random number is generated anew for each value of *j*. The factors τ and τ' are commonly set to $(\sqrt{2\sqrt{n}})^{-1}$ and $(2\sqrt{n})^{-1}$.

- 5) Calculate the fitness of each offspring $(x'_i, \eta'_i), \forall i \in \{1, \dots, \mu\}$.
- 6) Conduct a pairwise comparison over the union of parents (x_i, η_i) and offspring (x'_i, η'_i) , $\forall i \in \{1, \dots, \mu\}$. For each individual, q opponents are chosen uniformly at random from all the parents and offsprings. For each comparison, if the individual's fitness is not smaller than the opponent's, it will receive a "win".
- 7) Select μ individuals out of (x_i, η_i) and (x'_i, η'_i) , $\forall i \in \{1, \ldots, \mu\}$, that have the most wins to be the parents of the next generation.
- 8) Stop if the halting criterion is satisfied; otherwise, k = k + 1 and go to Step 3.

Many variants of EP have attempted to boost performance of the CEP [8-13]. They have usually changed Equations (1) and (2) in Step 3. Yao et al. [8] proposed a Cauchy-mutation-based EP, called fast EP (FEP). Fast EP (FEP) is similar to CEP, but uses a Cauchy function instead of a Gaussian function mutation as the primary search operator in Equations (1) and (2).

LEP (Levy distributed Evolutionary Programming) is a variant of EP, which is similar to CEP and FEP. The difference is in the mutation function; LEP uses a Levy distribution function in place of Gaussian for mutation function (Equation (2)) [9].

All three Gaussian, Cauchy, and Levy distribution functions are special cases of stable distributions. These distribution functions can be produced by Equation (3) in which x and y are Gaussian random numbers.

$$p = \frac{x}{y^{\frac{1}{\alpha}}}$$
(3)
if $\alpha = 2 \Rightarrow p$ is Guassian random number
if $\alpha = 1 \Rightarrow p$ is Cauchy random number
if $1 < \alpha < 2 \Rightarrow p$ is Levy random number

Three algorithms CEP, FEP and LEP are the most famous algorithms inside the EP family and new introduced variants are usually compared with these algorithms. For an in-depth review on EP variants, refer to [10].

3. The Proposed Method: Weighted Mean Classical Evolutionary Programming (WMCEP). Conceptually, each individual of one generation can be considered as a person looking for the coordinate of an unknown place (the global minimum). Each individual would want to approach a point, which does not have any previous records, information, or maps. The winner, which is named "the best individual", is the individual who can achieve the best estimation of the coordinate. Individuals are ranked according to their closeness to the global minimum, sorting individuals from low to high cost. At the end of each iteration, after a big tournament between new individuals and parents, some of the individuals are discarded because of their low ranks. It is necessary to say that parents are those who have won the last iteration. This is the approach of CEP, which may be regarded as blind searching.

When the new individual enters the tournament, the logical decision is to use the remaining information from the previous searching team (parents). If parents have found the proper region with low cost, it is advisable to search the same area and recede from areas that have high costs. However, care must be taken for avoiding trapping inside the local minimum. This approach is similar to the method called MCEP (Momentum Coefficient Evolutionary Programming) recently proposed in [6]. However, MCEP uses only the location of parents, and not their costs. One disadvantage of disregarding the cost of parents is pulling both best and worst individuals toward the same region. This means that best individuals do not have the opportunity to search their own area. Our scope in this paper is to add the information of individuals costs in determining the mean point by steering offspring toward the best individuals' area (those with best costs) and prevent them from getting close to the worst ones. Figure 1 shows this strategy.

For implementing this idea (Figure 1), two changes have been performed on CEP: 1) Weighted Mean Point (WMP) is defined as an estimation of the global minimum and 2) An approach similar to state feedback is used for steering offspring toward WMP.



FIGURE 1. Steering the offspring toward Weighted Mean Point (WMP). Ellipses are contours of a cost function with one global minimum.

3.1. Determining the WMP. In the proposed method, individuals are ranked using their cost; then a weight is allotted for each individual according to its rank. The individual that has the best cost attains a higher weight than others do, and vice versa. Thus, the proposed method introduces the weighted average of individuals for determining the location of WMP. Equation (4) shows the procedure of calculating WMP. Figure 2 shows a curve of weight versus rank, which is used in this study. Weighting leads WMP closer to the individuals with higher ranks. Therefore, they have more shares in determining the place of WMP. Steering the offspring toward WMP causes the offspring to move toward the best individuals, and prevents them from getting close to the parents with low ranks (Figure 1). By increasing the slope of curve in Figure 2, WMCEP becomes more elite, which may cause it to be trapped inside the local minimums.

$$Wmean = \sum_{i=1}^{n} w_i x_i, \quad \sum_{i=1}^{n} w_i = 1, \quad w_1 \ge w_2 \ge \ldots \ge w_\mu > 0 \tag{4}$$

where

$$w_{i} = \frac{e^{a(i)}}{\sum_{i=1}^{n} e^{a(i)}}$$
$$a(i) = 3 - \frac{i \times 6}{n}$$

where n is the population size.



FIGURE 2. Curve of weights via the individual's rank



FIGURE 3. WMCEP extends the offspring region by steering the offspring toward WMP

WMCEP extends the offspring region by steering the offspring toward WMP. Figure 3 shows the breeding region in the WMCEP algorithm. This region is larger than the region defined for CEP (see Figure 4). Thus, it is more probable that the global minimum is located inside the WMP region (depicted in Figure 3) and the probability of reaching the global minimum is more than other EP variants (see Figure 4). Figure 5 shows the offspring that was produced in the region near WMP.

Figure 5 shows that steering toward WMP can increase the convergence speed and accuracy of the method. Nevertheless, producing all offspring near WMP can lead to falling inside local minimums. Thus, the breading region must be controlled. The region near the parent is more robust against falling into local minimums, because in this region the step size for changing the offspring is small and most offspring are produced near their own parents; however, searching speed is very low (see Figure 4). On the other hand, the region near WMP gives a big step size for the offspring and, as a result, increases the



FIGURE 4. In the conventional EP, offspring is produced using the information of its own parent [6]



FIGURE 5. The results of WMCEP in producing offspring by steering them toward the weighted mean point of the parents

speed of the algorithm; however, it may cause trapping inside the local minimum, because most of the offsprings are produced in a small area near to WMP (see Figures 2 and 5). Consequently, the optimal region must be selected between parents and WMP regions. State feedback determines this optimal region.

3.2. Designing state feedback controller. WMCEP faces two challenges: 1) The weighted mean point may be far from the global minimum in the last iterations (if it falls in the local minimum, then it will mislead the offspring), and 2) speeding up the algorithms can cause premature convergence. The method that is more capable has more speed while it avoids being trapped in local minimums.

Using information has been obtained from the previous iteration can simultaneously fulfill both criteria of speed and accuracy. For solving both introduced issues, the speed of the algorithm must be controlled while getting close to the WMP. A controller similar to state feedback controls regions for breeding.

State feedback is a terminology used in control engineering (see block diagram in Figure 6).



FIGURE 6. Block diagram of the state feedback controller

State feedback is a kind of controller in which states of the system are measured and the control signal is produced by feedback gain. In state feedback, the value of the state vector is fed back to the input of the system. State feedback has an input, r, and defines the following relationship [11]:

$$u(t) = r(t) + Kx(t) \tag{5}$$

K is a constant matrix that is external to the system.

The searching process of EAs can be defined using the control block diagram. Figure 7 shows the searching scheme of conventional EAs which is similar to the open loop configuration. In this scheme, there is no control and feedback on the searching process.



FIGURE 7. Block diagram of conventional EAs searching process

WMP is far from the global minimum in the first iterations, but gets closer to it over time provided the algorithm be not trapped in local minimum. Hence, WMP can be used as the estimated coordinate of the global minimum. This estimation can be used as a basis for drawing feedback and designing the state feedback controller. Figure 8 shows the diagram of this process.

Similar to Equation (5), the controller similar to state feedback can be defined for WMCEP. Therefore, the offspring can be produced by Equation (6).

$$x'_{i}(j) = x_{i}(j) + \eta_{i}(j)N_{j}(0,1) + K \times WMP(j)$$
(6)

where the WMP(j) is the j element of WMP coordination. Now, the value of k must be determined. In state feedback, the value of K is extremely dependent on the system.



FIGURE 8. Block diagram of the state feedback control used in WMCEP

Consequently, the value of K in Equation (6) depends on the shape of cost functions. This dependence damages the generality of the algorithm. However, this value can be designed in such a way to be suitable for most kinds of cost functions (Equations (7) and (8)). Coefficient S is used for avoiding producing points out of the variable's boundaries. Thus, consider S + K = 1. Then,

$$x'_{i}(j) = S \times x_{i}(j) + \eta_{i}(j)N_{j}(0,1) + K \times Wmean(j)$$

$$\tag{7}$$

$$S = \frac{(total \; iter - iter)}{total \; iter}, \quad K = \frac{iter}{total \; iter} \tag{8}$$

In Equation (8), *total iter* is the abbreviation for the total number of iterations, which is specified by the user, and *iter* is the abbreviation for the current iteration.

Equation (8) introduces descending and ascending coefficients S and K. Defining S and K by (8) has some advantages. In the first iterations, the algorithm does not have any estimation of the global minimum, so as far as WMP is considered as the initial destination, the offspring can be given a known target. Consequently, speed can be increased by steering offsprings toward this destination. This is a goal of introducing WMP, but over time, the algorithm can find its way toward the global minimum. Therefore, by defining the descending coefficient for the weighted mean value (K in Equation (8)); the effectiveness of the WMP will be decreased. This strategy enables the algorithm to change its way toward the global minimum after finding good estimation of the global minimum. In other words, over time, the necessity for the weighted mean value decreases and the algorithm is able to find points near the global minimum.

At first glance, it may seem that this strategy is only possible when the global minimum is in the center of the search plate. However, searching with a high number of individuals helps in contemplating on all parts of the map simultaneously. The results of this paper indicate that this method is capable of finding the global minimum located anywhere on the search map.

In brief, WMCEP has two main differences with CEP: 1) Giving weights to the individuals by their rank, and defining WMP, which is the weighted average of the individual's location, and 2) Controlling the region of breeding offspring with regard to WMP. Therefore, the pseudo code of WMCEP is as follows.

Choose the initial population of individuals

Produce strategy parameters by any mutation function

Evaluate the cost of each individual in that population

Repeat this generation until termination: (time limit, sufficient cost achieved, etc.)

Rank individuals using their cost and give them weights

Update the weighted mean point using (4)

Breed individuals through mutation (Equation (7)) to give birth to the offspring Evaluate the cost of the offspring Raise tournament to decide the next generation members End

Figure 9 shows the flowchart of WMCEP.



FIGURE 9. Flowchart of WMCEP

4. **Results.** Nine algorithms of CEP, FEP [8], LEP [9], EEP (Exponential Evolutionary Programming) [12], RLEP (Evolutionary Programming based on Reinforcement Learning) [13], CMA-ES [7], JG-GA (Jumping Gene GA) [14,15], IW-PSO (Increasing Inertia Weight PSO) [16] and WMCEP are compared in this section. These algorithms consist of two groups: algorithms are and are not considered as evolutionary programming variants. An attempt has been made to select the algorithms, which are known in and out of their own families and have some similarities to the proposed method. No attempt was made to optimize algorithms against cost functions.

Table 1 shows the name and references of cost functions. Their parameters, dimensions and variable bounds are the same as the references. The source codes of these cost functions are available in [17]. A detailed explanation of cost functions can be found in the references cited in Table 1. All parameters of the algorithms are the same as introduced in Table 2.

The algorithms have been tested on the 65 cost functions. Each test has been repeated 50 times and the average results are shown in Table 3. This table compares the accuracy of the methods in obtaining the global minimum.

Distances between the optimal points found by WMCEP and other algorithms show that the performance of the proposed method is notable. This can be an effect of implementing the strategy of using information of the best individual's costs and locations in producing offspring.

Cost	Name	Dimension (n)	Bounds	Global	Reference
F1	Snhere Model	10	$[-10, 10]^n$	65	[18]
F2	Ellipsoidal Function	10	$[-10, 10]^n$	276 32	[10]
F3	Bastrigin Function	10	$[-10, 10]^n$	20.91	[18]
F4	Buche-Bastriain Function	10	$[-10, 10]^n$	20.91	[10]
F5	Linear Slone	10	$[-10, 10]^n$	51 53	[10]
F6	Attractive Sector Function	10	$[-10, 10]^n$	83 48	[18]
F7	Sten Ellinsoidal Function	10	$[-10, 10]^n$	-83.87	[10]
F8	Rosenbrock Function original	10	$[-10, 10]^n$	-135	[18]
F9	Rosenbrock Function rotated	10	$[-10, 10]^n$	-359	[18]
F10	Ellipsoidal Function	10	$[-10, 10]^n$	-78.98	[18]
F11	Discus Function	10	$[-10, 10]^n$	-101	[10]
F12	Bent Cigar Function	10	$[-10, 10]^n$	295.1	[10]
F12 F13	Sharp Ridge Function	10	$[-10, 10]^n$	-51.73	[18]
F14	Different Powers Function	10	$[-10, 10]^n$	57.00	[10]
F14 F15	Bastriain Function	10	$[-10, 10]^n$	-31.30	[10]
F15 F16	Weienstrass Function	10	$[-10, 10]^n$	-44.11	[10]
F10 F17	Schaffers F7 Function	10	[-10, 10] $[-10, 10]^n$	-200	[10]
F17 F19	Schaffere F7 Exaction moderately ill conditioned	10	[-10, 10]	-38.72	[10]
F10	Composite Crisewanh Possenbrook Eurotion F8F0	10	$[-10, 10]^n$	-30.12	[10]
F 19 F 20	Composite Griewank-Rosenorock Function F8F2	10	[-10, 10]	40.40	[10]
Г20 Г91	Callacher's Caussian 101 mg Books Function	10	$[-10, 10]^n$	210.6	[10]
Г 41 Г 22	Gallagher's Gaussian 101-me Feaks Function	10	$[-10, 10]^n$	310.0 42.07	[10]
F 22	Guilagner's Guissian 21-ni Feaks Function	10	$[-10, 10]^n$	42.97	[10]
Г 20 F24	Kalsuura Function	10	$[-10, 10]^n$	210.4	[10]
Г <u>4</u> 4 Бог	Conservational Coloured Republication	10	[-10, 10]"	47.50	[10]
F 20 F20	Generalized Schwefel's Problem 2.20	30	$[-500, 500]^n$	-12569.5	[8]
F 20	Generalized Rastrigin's Function	30	$[-0.12, 0.12]^n$	0	[8]
F 27	Ackiey's Function	30	$[-32, 32]^n$	0	[8]
F28	Generalized Griewank Function	30	$[-600, 600]^n$	0	[8]
F 29	Generalized Penalized Functions	30	$[-50, 50]^n$	0	[8]
F 30	Generalized Penalized Functionsz	30	$[-50, 50]^n$	0	[8]
F31 590	Snekel's Foxnoles Function	2	$[-05.53, 05.53]^{-1}$	1	[8]
Г 3 <i>4</i> Б 9 9	Cin House Court Back Function	4	$[-3, 5]^n$	1.0216285	[0]
F 33	Six-Hump Camel-Back Function	2	$[-3, 3]^{-1}$	-1.0316285	[8]
F 34	Branin Function	2	$[-5, 10] \times [0, 15]$	0.398	[8]
F35	Goldstein-Price Function	2	$[-2, 2]^n$	3	[8]
F36	Hartman's Family1	3	$[0, 1]^n$	-3.86	[8]
F37	Hartman's Family2	6	$[0, 1]^n$	-3.32	[8]
F38 E20	Shekel's Family1	4	$[0, 10]^n$	-10	[8]
F 39	Shekel's Family2	4	$[0, 10]^n$	-10	[8]
F40	Shekel's Family3	4	$[0, 10]^n$	-10	[8]
F41	Corana's parabola	4	$[-1000, 1000]^n$	0	[19]
F42	deceptive function	10	$[0, 1]^n$	-16	[19]
F43	Sum of different power	30	$[-1, 1]^n$	0	[20]
F44	Beale function	10	$[-5,10]^{n}$	0	[20]
F45	Alpine function	10	$[-10, 10]^n$	0	[20]
F46	Inverted cosine wave function (Masters)	10	[-5,5]"	$\frac{-n+1}{2}$	[20]
F47	Hyper-Ellipsoid	10	$[-100, 100]^n$	0	[21]
F48	Neumaier #3	30	$[-900, 900]^n$	-4930	[21]
F49	Salomon	10	$[-10, 10]^n$	0	[21]
F 50	Lennara-Jones	10	$[-2, 2]^{n}$	1 1 4 9 9 9	[21]
F 51	Vaa Square	20	$[-5\pi, 5\pi]^n$	-1.14383	[21]
F52	Katsuura	10	[-1000, 1000]"	1	[21]
F 5 3	Bonacnevský i Problem (BF1)	2	$[-50, 50]^{n}$	0	[22]
F 54	Camel Back – 3 Inree Hump Problem (CB3)	2	$[-3, 3]^n$	0	[22]
1755 1750	Cosine Mixture Problem (UM)	10	$[-100, 100]^{\prime\prime}$	- 1	[22]
F 30	Eusom Proolem (EP)	2	$[-10, 10]^n$		[22]
1°57 1750	Epistatic Michalewicz Problem (EM)	10	$[0,\pi]^{n}$	-9.060152	[22]
F58	Exponential Problem (EXP)	30	$[-1, 1]^n$	-1	[22]
F59	Meyer and Koth Problem (MK)	చ ం	$[-10, 10]^{n}$	0.00004	[22]
F60	Modified Kosenbrock Problem (MRP)	2	$[-5, 5]^{n}$	U 1.00205	[22]
F61	Multi-Gaussian Problem (MGP)	2	$[-2, 2]^n$	1.29695	[22]
F62	Paviani Problem (PP)	10	$[2, 10]^n$	-45.778	[22]
F63	Schaffer 2 Problem (SF2)	2	$[-10, 10]^n$	0	[22]
F'64	Shubert Problem (SBT)	2	$[-10, 10]^n$	-186.7309	[22]
F'65	Sinusoidal Problem (SIN)	10	$[0, 180]^n$	-3.5	[22]

TABLE 1. Description of the sixty-five cost functions used in this study

	Population size	100	
Gonoral	Number of repetition	50	
General	Tournament size q	10	
	Initial standard deviation	3	
FEP	Parameter t for Cauchy distribution function	1	
LEP	Value of α for Levy distribution function in Equation (3)	1.5	
CMA-ES	All parameters are similar to the source codes in [8]		
	Number of transposon	1	
JG	Length of transposon	2	
	crossover	Uniform	
	Mutation rate	0.1	
	Acceleration coefficients	2	
IW-PSO	Linearly increasing inertia weight	From 0.5 to 1.5	
	Maximum velocity	$\pm X_{max}$	

TABLE 2. Parameters of evolutionary programming's variants

It must be noticed that the RLEP is a fast and accurate algorithm, which produces offspring by predicting the future performance of the algorithm. However, it needs many calculations and evaluates many cost functions (at least four times more than CEP). Therefore, in all comparisons of this paper, all the algorithms were run until the prespecified number of cost functions was evaluated.

5. Statistical Test. In recent years, use of statistical tests for improving performance evaluation of a new method has become a widespread technique in computational intelligence. In this section, a procedure is assigned to estimate the differences between several algorithms. It is named the Contrast Estimation of Medians method. This method is very recommendable if assumed that the global performance is reflected by the magnitudes of differences between performances of the algorithms [23]. These estimators can be understood as an advanced global performance measure. It is especially useful to estimate the extent to which an algorithm outperforms another one [23].

In the current experimental analysis, the set of estimators of medians is calculated directly from the average error results. Table 8 shows the estimations computed for each algorithm. This comparison was performed in two groups: inside and outside of the EP family. By focusing attention on the rows of the table, the performance of WMCEP may be highlighted (all its related estimators are negative, i.e., it achieves very low error rates considering median estimators). On the other hand, FEP achieves higher error rates in this experimental study. Table 4 shows that WMCEP is most similar to CMA-ES in error rate (performance), as the Contrast estimated method shows small difference between error rate of WMCEP and CMA-ES. Thus, in next step, WMCEP and CMA-ES are compared in terms of performance in more detail.

6. Comparing WMCEP and CMA-ES. In this section, the two algorithms of WM-CEP and CMA-ES are compared in detail. CPU times and their sensitivities to variable bounds, number of population and cost function dimensions are the issues of this section.

6.1. **CPU time.** It is predictable that CMA-ES requires more CPU time. This algorithm has more complicated equations and needs many calculations [7]. Two algorithms, WMCEP and CMA-ES, were tested on a 30 dimensional cost function. An iteration of CMA-ES needs, in average, 0.0272 seconds, while WMCEP requires 0.012 seconds.

TABLE 3. Results of 50 repetitions of testing algorithms on $65 \cos t$ functions

	CEP	FEP	LEP	EEP	BLEP	CMAES	IIW-PSO	GA-JG	WMCEP	Global	Generation
F1	525.0	-18.63	-37.83	-92.17	-91.70	-92.64	-90.94	-88.24	-92.64	-92.65	100
F2	27634	25192	70705	1016.9	515.24	276.32	11728	3728	276.32	276.32	100
F3	723	70.60	57.60	42.75	37.73	25.08	111.8	94.32	23.29	20.91	500
F4	53.96	906.2	35.19	24.88	27.11	30.85	133.6	117.2	29.77	20.91	500
F5	51.53	51.53	51.53	51.53	51.97	62.52	53.92	53.41	51.53	51.53	50
F6	2189	1883	86.06	102.4	85.46	83.48	144.7	112.3	83.49	83.48	500
F7	5052	1516	1.501	-61.07	-64.27	-83.87	-54.94	-63.69	-82.22	-83.87	100
F8	-10.29	1402	-3.37	-127.6	-120.8	-135	-113.2	153.5	-128.5	-135	500
F9	-349	800231	3646	-268.3	-250	-359.2	-318.1	-324.5	-351.2	-359	200
F10	80977	48179	70459	3940.2	886.51	-78.98	538.5	7664.5	975	-78.98	5000
F11	-7.05	20.29	-33.01	52.92	14.68	-101	-92.82	-56.44	-59.77	-101	1000
F12	342	11742	337	379.8	7225.8	295.1	341.8	1.8e + 6	299.6	295.1	500
F13	-6.32	17.77	-34.99	-48.47	-28.21	-51.73	-24.41	157	-51.15	-51.73	1000
F14	-57.87	-57.07	-57.84	-57.83	-56.40	-57.9	-57.87	-56.40	-57.9	-57.90	200
F15	-20.57	9.955	-30.84	-15.91	-36.59	-42.87	7.067	27.61	-41.57	-44.77	1000
F16	-257.5	-252.4	-257.4	-258.3	-258.4	-256.2	-254.9	-252.8	-259.3	-260	1000
F17	-37.25	-36.11	-38.29	-38.15	-38.22	-38.72	-36.59	-36.65	-38.60	-38.72	200
F18	-37.11	-29.53	-37.97	-37.89	-36.02	-38.72	-33.88	-33.46	-37.60	-38.72	500
F19	42.40	42.19	42.09	41 54	42.63	40.63	42.80	42.54	42.21	40.46	300
F20	1.842	215.8	18/	18/	185.2	18/	18/	12.01	18/	183.1	200
F21	310.6	311.5	310.6	310.6	311.8	317	318	322	310.6	310.6	500
F22	53 33	46.54	45.18	52 57	45 78	58.10	57 19	52.22	47.96	42.97	500
F23	211.7	210.5	211.7	211.7	211.7	210.5	210.8	211.5	211.4	210.4	3000
F24	67.57	107.4	72.81	78.83	71.22	56.837	210.0	100	56 318	47.56	1000
F25	-8455	-12/93	-12351	-11026	-11878.2	-2572	-8917	-7040	-8384	-12569.5	3000
F26	57.01	6 76	98.59	369.6	106.8	8.06	73 77	1040	5 57	0	3000
F27	6 36	1.13	0.26	20.01	1 8/12	8e – 15	5	5.14	5e - 12	0	3000
F28	8.16	1.13	0.20	3 31	0.928	0	1.03	2 32	0	0	3000
F29	15.65	0.66	0.002	2 42	0.149	21.74	18.52	3.32	1.54e - 24	0	3000
F30	62.60	10.32	0.16	86.38	0.020	1 20	31.6	13.30	9.7e - 26	0	3000
F31	1	1	1	1 246	1	2.98	1	10.00	1	1	2000
F32	0.006	0.01	0.005	0.003	0.0056	0.01	0.02	0.006	0.004	0.0003075	400
F33	-1 0316	-1.0316	-1.0316	-1.0316	-1 0316	-0.99	-1.031	-1.030	-1.031	-1.0316285	100
F34	0.397	0.397	0.397	0.397	0.397	0.397	0.397	0.397	0.397	0.397	100
F35	3	3	3	3	3	3	3	3	3	3	100
F36	-3.86	-3.86	-3.86	-3.86	-3.86	-3.862	-3.862	-3.862	-3.862	-3.86	100
F37	-3 298	-3.298	-3.274	-3.25	-3.32	-3.31	-3.28	-3.28	-3.26	-3.32	500
F38	-10.15	-10.15	-10.15	-7.17	-10.15	-5.74	-8.13	-7.31	-8.2	-10	100
F39	-9.50	-8.82	10110		10110	0.1.1	0.10	1101	0.2	10	100
F40	0.00		-9.01	-7.86	-8.91	-6.58	-8.43	-9.26	-9.47	-10	100
F41	-9.15	-8.71	-9.01 -9.90	-7.86 -8.55	-8.91 -9.60	-6.58 -5.73	-8.43 -7.41	-9.26 -9.59	-9.47 -10.52	-10 -10	100 100
	-9.15 0	-8.71 0	-9.01 -9.90 0	-7.86 -8.55 0	-8.91 -9.60 0	-6.58 -5.73 3.957	-8.43 -7.41 0	-9.26 -9.59 0	$-9.47 \\ -10.52 \\ 0$	-10 -10 0	100 100 1000
F42	-9.15 0 -16	-8.71 0 -15.81	-9.01 -9.90 0 -12.33	-7.86 -8.55 0 -16	-8.91 -9.60 0 -13.55	-6.58 -5.73 3.957 -5.12	-8.43 -7.41 0 -16	-9.26 -9.59 0 -13.65	-9.47 -10.52 0 -16	-10 -10 0 -16	100 100 1000 1000
F42 F43	-9.15 0 -16 2.76e - 39	-8.71 0 -15.81 1.09e - 18	$ \begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ \end{array} $	-7.86 -8.55 0 -16 3.4e - 34	-8.91 -9.60 0 -13.55 5.21e - 5	$ \begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \end{array} $	-8.43 -7.41 0 -16 1 1e - 12	-9.26 -9.59 0 -13.65 1.54e - 8	-9.47 -10.52 0 -16 1.1e - 82	-10 -10 0 -16 0	100 100 1000 1000 3000
F42 F43 F44	-9.15 0 -16 2.76e - 39 7.15e - 6	-8.71 0 -15.81 1.09e - 18 1.15	$ \begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ \hline 0.003 \\ \end{array} $	-7.86 -8.55 0 -16 3.4e - 34 0.0011	$ \begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ \hline 5.21e - 5 \\ 0.0010 \\ \end{array} $	$ \begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ \end{array} $	-8.43 -7.41 0 -16 1.1e - 12 3.8e - 4	-9.26 -9.59 0 -13.65 1.54e - 8 0.06	$ \begin{array}{r} -9.47 \\ -10.52 \\ 0 \\ -16 \\ 1.1e - 82 \\ 1e - 07 \\ \end{array} $	-10 -10 0 -16 0 0	$ \begin{array}{r} 100 \\ 100 \\ 1000 \\ 3000 \\ 1000 \end{array} $
F42 F43 F44 F45	-9.15 0 -16 2.76e - 39 7.15e - 6 4.38e - 15	-8.71 0 -15.81 1.09e - 18 1.15 0.016	$ \begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ \hline 0.003 \\ \hline 0.003 \\ \hline 5e - 16 \\ \end{array} $	-7.86 -8.55 0 -16 3.4e - 34 0.0011 4.1e - 15	$ \begin{array}{r} -8.91 \\ -9.60 \\ 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ \end{array} $	$ \begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ \end{array} $	-8.43 -7.41 0 -16 1.1e - 12 3.8e - 4 0.1	$ \begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ \hline 0.06 \\ 0.007 \\ \end{array} $	$ \begin{array}{r} -9.47 \\ \hline -10.52 \\ 0 \\ \hline -16 \\ 1.1e - 82 \\ 1e - 07 \\ 6.9e - 19 \\ \end{array} $	-10 -10 0 -16 0 0 0	100 100 1000 1000 3000 1000
F42 F43 F44 F45 F46	-9.15 0 -16 2.76e - 39 7.15e - 6 4.38e - 15 -7.191	-8.71 0 -15.81 1.09e - 18 1.15 0.016 -8.333	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ \hline 0.003 \\ \hline 5e - 16 \\ -8.257 \end{array}$	$-7.86 \\ -8.55 \\ 0 \\ -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ -8.341 \\ $	$-8.91 \\ -9.60 \\ 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ -8.341$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ \hline 1e - 126 \\ 3.2e - 14 \\ -5.16 \end{array}$	$-8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ $	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \end{array}$	$-9.47 \\ -10.52 \\ 0 \\ -16 \\ 1.1e - 82 \\ 1e - 07 \\ 6.9e - 19 \\ -8.34$	$ \begin{array}{r} -10 \\ -10 \\ 0 \\ -16 \\ 0 \\ 0 \\ 0 \\ -n+1 \\ \end{array} $	100 100 1000 1000 3000 1000
F42 F43 F44 F45 F46 F47	-9.15 0 -16 2.76e - 39 7.15e - 6 4.38e - 15 -7.191 6.53e - 12	-8.71 0 -15.81 1.09e - 18 1.15 0.016 -8.333 14.67	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ \hline 0.003 \\ \hline 5e - 16 \\ -8.257 \\ \hline 3e - 13 \end{array}$	$-7.86 \\ -8.55 \\ 0 \\ -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ -8.341 \\ 9.61e - 6$	$-8.91 \\ -9.60 \\ 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ 3.79e - 6$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \end{array}$	$-8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ -8.42$	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \end{array}$	$ \begin{array}{r} -9.47 \\ -10.52 \\ 0 \\ \hline 1.1e - 82 \\ 1e - 07 \\ \hline 6.9e - 19 \\ \hline -8.34 \\ 1.1e - 43 \\ \end{array} $	$ \begin{array}{r} -10 \\ -10 \\ 0 \\ -16 \\ 0 \\ 0 \\ 0 \\ -n+1 \\ 0 \\ \end{array} $	$ \begin{array}{r} 100 \\ 100 \\ 1000 \\ 3000 \\ 10$
F42 F43 F44 F45 F46 F46 F47 F48	-9.15 0 -16 2.76e - 39 7.15e - 6 $4.38e - 15$ -7.191 $6.53e - 12$ 270736	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \end{array}$	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ 5e - 16 \\ -8.257 \\ 3e - 13 \\ 18935 \end{array}$	$\begin{array}{r} -7.86 \\ -8.55 \\ \hline 0 \\ \hline -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ \hline -8.341 \\ 9.61e - 6 \\ 127880 \end{array}$	$-8.91 \\ -9.60 \\ 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ 3.79e - 6 \\ 5951 \\ -8.951 \\ $	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \end{array}$	$-8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ $	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \\ 21654 \end{array}$	$\begin{array}{r} -9.47 \\ -10.52 \\ 0 \\ \hline 1.1e - 82 \\ 1e - 07 \\ 6.9e - 19 \\ \hline -8.34 \\ 1.1e - 43 \\ -1053 \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930	100 100 1000 1000 3000 1000 1000 1000 1000 1000 3000
F42 F43 F44 F45 F46 F47 F47 F48 F49	$\begin{array}{r} -9.15 \\ \hline 0 \\ \hline 2.76e - 39 \\ \hline 7.15e - 6 \\ 4.38e - 15 \\ \hline -7.191 \\ 6.53e - 12 \\ 270736 \\ \hline 0.195 \end{array}$	-8.71 0 -15.81 1.09e - 18 1.15 0.016 -8.333 14.67 51291 0.980	$\begin{array}{r} -9.01 \\ \hline -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ 5e - 16 \\ -8.257 \\ 3e - 13 \\ 18935 \\ 0.190 \end{array}$	$\begin{array}{r} -7.86 \\ -8.55 \\ \hline 0 \\ -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ -8.341 \\ 9.61e - 6 \\ 127880 \\ 0.599 \end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ \hline -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ \mathbf{1e} - 126 \\ 3.2e - 14 \\ -5.16 \\ \mathbf{1e} - 121 \\ -4930 \\ 0.14 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ \hline 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \end{array}$	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \\ 21654 \\ 0.22 \end{array}$	$\begin{array}{r} -9.47 \\ -10.52 \\ 0 \\ -16 \\ 1.1e - 82 \\ 1e - 07 \\ 6.9e - 19 \\ -8.34 \\ 1.1e - 43 \\ -1053 \\ 0.10 \end{array}$	$\begin{array}{c} -10 \\ -10 \\ 0 \\ \hline 0 \\ 0 \\ 0 \\ -n+1 \\ 0 \\ -4930 \\ 0 \\ \end{array}$	100 100 1000 3000 1000 1000 1000 1000 1
F42 F43 F44 F45 F46 F47 F48 F49 F50	-9.15 0 -16 2.76e - 39 7.15e - 6 4.38e - 15 -7.191 6.53e - 12 270736 0.195 -5.288	-8.71 0 -15.81 1.09e - 18 1.15 0.016 -8.333 14.67 51291 0.980 -5.286	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ 5e - 16 \\ -8.257 \\ 3e - 13 \\ 18935 \\ 0.190 \\ -5.288 \end{array}$	-7.86 -8.55 0 -16 3.4e - 34 0.0011 4.1e - 15 -8.341 9.61e - 6 127880 0.599 -5.11	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ \hline -8.341 \\ 3.79e - 16 \\ 5.951 \\ 0.199 \\ -4.07 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ \hline 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \end{array}$	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \\ 21654 \\ 0.22 \\ -4.73 \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e-82\\ 1e-07\\ 6.9e-19\\ -8.34\\ 1.1e-43\\ -1053\\ 0.10\\ -5.28\end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 -	$\begin{array}{c} 100\\ 100\\ 1000\\ 1000\\ 1000\\ 1000\\ 1000\\ 1000\\ 1000\\ 1000\\ 1000\\ 1000\\ 1000\\ 1000\\ \end{array}$
F42 F43 F44 F45 F46 F47 F48 F49 F50 F51	$\begin{array}{r} -9.15\\ \hline 0\\ \hline -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\end{array}$	-8.71 0 -15.81 1.09e - 18 1.15 0.016 -8.333 14.67 51291 0.980 -5.286 -3.2e - 13	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ 5e - 16 \\ -8.257 \\ 3e - 13 \\ 18935 \\ 0.190 \\ -5.288 \\ -0.06 \end{array}$	$\begin{array}{r} -7.86 \\ -8.55 \\ \hline 0 \\ -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ -8.341 \\ 9.61e - 6 \\ 127880 \\ 0.599 \\ -5.11 \\ -2.3e - 7 \end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ \hline -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ 0 \\ \mathbf{-16} \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ \mathbf{-5.28} \\ -0.001 \end{array}$	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \\ 21654 \\ 0.22 \\ -4.73 \\ -2.5e - 4 \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e-82\\ 1e-07\\ 6.9e-19\\ -8.34\\ 1.1e-43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 - -1.14383	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 2000
F42 F43 F44 F45 F46 F47 F48 F49 F50 F51 F52	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \end{array}$	$\begin{array}{r} -9.01 \\ -9.90 \\ 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ 5e - 16 \\ -8.257 \\ 3e - 13 \\ 18935 \\ 0.190 \\ -5.288 \\ -0.06 \\ 1 \end{array}$	-7.86 -8.55 0 -16 3.4e - 34 0.0011 4.1e - 15 -8.341 9.61e - 6 127880 0.599 -5.11 -2.3e - 7 4.093	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ \hline -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ \hline \mathbf{1e} - 126 \\ 3.2e - 14 \\ -5.16 \\ \hline \mathbf{1e} - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ \hline 1 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ 0 \\ \mathbf{-16} \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ \mathbf{-5.28} \\ -0.001 \\ 5e + 11 \end{array}$	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \\ 21654 \\ 0.22 \\ -4.73 \\ -2.5e - 4 \\ 3.4e + 10 \end{array}$	$\begin{array}{r} -9.47 \\ -10.52 \\ 0 \\ -16 \\ 1.1e - 82 \\ 1e - 07 \\ 6.9e - 19 \\ \hline -8.34 \\ 1.1e - 43 \\ -1053 \\ 0.10 \\ -5.28 \\ -0.63 \\ 1 \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 -1.14383 1	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 2000 1000
$\begin{array}{c} F42 \\ F43 \\ F44 \\ F45 \\ F46 \\ F47 \\ F48 \\ F49 \\ F50 \\ F51 \\ F52 \\ F53 \\ \end{array}$	$\begin{array}{r} -9.15 \\ \hline 0 \\ -16 \\ 2.76e - 39 \\ 7.15e - 6 \\ 4.38e - 15 \\ -7.191 \\ 6.53e - 12 \\ 270736 \\ 0.195 \\ -5.288 \\ -0.03 \\ \hline 1 \\ 5.4e - 13 \end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \end{array}$	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ \overline{5e-16} \\ -8.257 \\ \overline{3e-13} \\ 18935 \\ 0.190 \\ -5.288 \\ -0.06 \\ \hline 1 \\ \overline{5e-12} \end{array}$	-7.86 -8.55 0 -16 3.4e - 34 0.0011 4.1e - 15 -8.341 9.61e - 6 127880 0.599 -5.11 -2.3e - 7 4.093 5.5e - 17	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e-5 \\ 0.0010 \\ 2.54e-16 \\ \hline -8.341 \\ 3.79e-6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \\ 2.96e-7 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ \textbf{0} \\ \textbf{-16} \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ \textbf{-5.28} \\ -0.001 \\ 5e + 11 \\ 2e - 5 \end{array}$	$\begin{array}{r} -9.26\\ -9.59\\ \hline 0\\ -13.65\\ 1.54e-8\\ 0.06\\ 0.007\\ -8.15\\ 26.84\\ 21654\\ 0.22\\ -4.73\\ -2.5e-4\\ 3.4e+10\\ 0.08\\ \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e-82\\ 1e-07\\ 6.9e-19\\ -8.34\\ 1.1e-43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 0\\ \end{array}$	$\begin{array}{c} -10 \\ -10 \\ 0 \\ -16 \\ 0 \\ 0 \\ 0 \\ -n+1 \\ 0 \\ -4930 \\ 0 \\ -1.14383 \\ 1 \\ 0 \\ \end{array}$	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000
$\begin{array}{c} F42 \\ F43 \\ F44 \\ F45 \\ F46 \\ F47 \\ F48 \\ F49 \\ F50 \\ F51 \\ F52 \\ F53 \\ F54 \end{array}$	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 5.4e-13\\ 2.03e-15 \end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \end{array}$	$\begin{array}{r} -9.01 \\ \hline -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ \overline{5e-16} \\ -8.257 \\ \overline{3e-13} \\ 18935 \\ 0.190 \\ \hline -5.288 \\ -0.06 \\ \hline 1 \\ 5e-12 \\ 2e-13 \end{array}$	$\begin{array}{r} -7.86 \\ -8.55 \\ \hline 0 \\ -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ \hline -8.341 \\ 9.61e - 6 \\ 127880 \\ 0.599 \\ -5.11 \\ -2.3e - 7 \\ 4.093 \\ 5.5e - 17 \\ 8.2e - 16 \end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ \hline -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ \hline 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \end{array}$	$\begin{array}{r} -9.26\\ -9.59\\ \hline 0\\ -13.65\\ 1.54e-8\\ 0.06\\ 0.007\\ -8.15\\ 26.84\\ 21654\\ 0.22\\ -4.73\\ -2.5e-4\\ 3.4e+10\\ 0.08\\ 5.4e-5\end{array}$	$\begin{array}{r} -9.47 \\ -10.52 \\ 0 \\ \hline 0 \\ -16 \\ 1.1e - 82 \\ 1e - 07 \\ 6.9e - 19 \\ \hline -8.34 \\ 1.1e - 43 \\ -1053 \\ \hline 0.10 \\ -5.28 \\ -0.63 \\ 1 \\ 0 \\ 1.1e - 26 \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 -1.14383 1 0 0 0	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 100 100
$\begin{array}{c} F42 \\ F43 \\ F44 \\ F45 \\ F46 \\ F47 \\ F48 \\ F49 \\ F50 \\ F51 \\ F52 \\ F53 \\ F54 \\ F55 \\ \end{array}$	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 5.4e-13\\ 2.03e-15\\ -10e+5\\ \end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \end{array}$	$\begin{array}{r} -9.01 \\ \hline -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ \hline 5e-16 \\ -8.257 \\ \hline 3e-13 \\ 18935 \\ 0.190 \\ \hline -5.288 \\ -0.06 \\ \hline 1 \\ 5e-12 \\ 2e-13 \\ -99987 \\ \end{array}$	$\begin{array}{r} -7.86 \\ -8.55 \\ \hline 0 \\ -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ \hline -8.341 \\ 9.61e - 6 \\ 127880 \\ 0.599 \\ -5.11 \\ -2.3e - 7 \\ 4.093 \\ 5.5e - 17 \\ 8.2e - 16 \\ -92418 \end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ -10e + 5 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ \end{array}$	$\begin{array}{r} -9.26\\ -9.59\\ \hline 0\\ -13.65\\ 1.54e-8\\ 0.06\\ 0.007\\ -8.15\\ 26.84\\ 21654\\ 0.22\\ -4.73\\ -2.5e-4\\ 3.4e+10\\ 0.08\\ 5.4e-5\\ -84095 \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e - 82\\ 1e - 07\\ 6.9e - 19\\ -8.34\\ 1.1e - 43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 0\\ 1.1e - 26\\ -99999\\ \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 -1.14383 1 0 0 - -1.14383 -	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 100 100 100
$\begin{array}{c} F42\\ F43\\ F44\\ F45\\ F46\\ F47\\ F48\\ F49\\ F50\\ F51\\ F52\\ F53\\ F54\\ F55\\ F56\\ F56\\ \end{array}$	$\begin{array}{r} -9.15 \\ \hline 0 \\ -16 \\ 2.76e - 39 \\ 7.15e - 6 \\ 4.38e - 15 \\ -7.191 \\ 6.53e - 12 \\ 270736 \\ 0.195 \\ -5.288 \\ -0.03 \\ \hline 1 \\ 5.4e - 13 \\ 2.03e - 15 \\ -10e + 5 \\ -10e + 5 \\ -10 \\ -1 \end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ -1 \end{array}$	$\begin{array}{r} -9.01 \\ \hline -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 5e - 16 \\ -8.257 \\ 3e - 13 \\ 18935 \\ 0.190 \\ \hline -5.288 \\ -0.06 \\ \hline 1 \\ 5e - 12 \\ 2e - 13 \\ -99987 \\ -1 \end{array}$	$\begin{array}{r} -7.86 \\ -8.55 \\ \hline 0 \\ -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ \hline -8.341 \\ 9.61e - 6 \\ 127880 \\ 0.599 \\ -5.11 \\ -2.3e - 7 \\ 4.093 \\ 5.5e - 17 \\ 8.2e - 16 \\ -92418 \\ -1 \end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ 8.72e - 9 \\ -10e + 5 \\ -1 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ 3.8e - 4 \\ 0.1 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \end{array}$	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \\ 21654 \\ 0.22 \\ -4.73 \\ -2.5e - 4 \\ 3.4e + 10 \\ 0.08 \\ 5.4e - 5 \\ -84095 \\ -1 \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e-82\\ 1e-07\\ 6.9e-19\\ -8.34\\ 1.1e-43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 0\\ 1.1e-26\\ -99999\\ -1\\ \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 -1.14383 1 0 0 - -1.14383 - -1	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 100 100 100 100 1000 1000
$\begin{array}{c} F42\\ F43\\ F44\\ F45\\ F46\\ F47\\ F48\\ F49\\ F50\\ F51\\ F52\\ F53\\ F54\\ F55\\ F56\\ F57\\ \end{array}$	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 5.4e-13\\ 2.03e-15\\ -10e+5\\ -10\\ -7.287\end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ -1 \\ -7.649 \end{array}$	$\begin{array}{r} -9.01 \\ \hline -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 5e - 16 \\ -8.257 \\ 3e - 13 \\ 18935 \\ 0.190 \\ \hline -5.288 \\ -0.06 \\ \hline 1 \\ 5e - 12 \\ 2e - 13 \\ -99987 \\ \hline -1 \\ -5.921 \\ \end{array}$	$\begin{array}{r} -7.86 \\ -8.55 \\ \hline 0 \\ -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ -8.341 \\ 9.61e - 6 \\ 127880 \\ 0.599 \\ -5.11 \\ -2.3e - 7 \\ 4.093 \\ 5.5e - 17 \\ 8.2e - 16 \\ -92418 \\ -92418 \\ -7.38 \\ \end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ -10e + 5 \\ -1 \\ -7.724 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \\ -4.4 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \\ -5.77 \end{array}$	$\begin{array}{r} -9.26\\ -9.59\\ \hline 0\\ -13.65\\ 1.54e-8\\ 0.06\\ 0.007\\ -8.15\\ 26.84\\ 21654\\ 0.22\\ -4.73\\ -2.5e-4\\ 3.4e+10\\ 0.08\\ 5.4e-5\\ -84095\\ -84095\\ -1\\ -5.47\end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e-82\\ 1e-07\\ 6.9e-19\\ -8.34\\ 1.1e-43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 0\\ 1.1e-26\\ -99999\\ -1\\ -7.67\\ \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 -1.14383 1 0 0 -1.14383 1 0 -1.143838 -1.143838 -1.14388 -1.14388 -1.14388 -1.14388 -1.14388 -1.14388 -1.14388 -1.14388 -1.14388 -1.14388 -1.14388 -1.143888	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 100 100 100 100 100 100 100
$\begin{array}{c} F422\\ F43\\ F44\\ F45\\ F46\\ F47\\ F48\\ F49\\ F50\\ F51\\ F52\\ F53\\ F54\\ F55\\ F56\\ F57\\ F58\end{array}$	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 5.4e-13\\ 2.03e-15\\ -10e+5\\ -1\\ -7.287\\ -0.98\\ \end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ \hline -1 \\ -7.649 \\ -0.974 \end{array}$	$\begin{array}{r} -9.01 \\ \hline -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 5e - 16 \\ -8.257 \\ 3e - 13 \\ 18935 \\ 0.190 \\ \hline -5.288 \\ -0.06 \\ \hline 1 \\ 5e - 12 \\ 2e - 13 \\ -99987 \\ \hline -1 \\ -5.921 \\ -0.17 \\ \end{array}$	$\begin{array}{r} -7.86\\ -8.55\\ \hline 0\\ -16\\ 3.4e-34\\ 0.0011\\ 4.1e-15\\ -8.341\\ 9.61e-6\\ 127880\\ 0.599\\ -5.11\\ -2.3e-7\\ 4.093\\ 5.5e-17\\ 8.2e-16\\ -92418\\ \hline -1\\ -7.38\\ -0.97\\ \end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ -10e + 5 \\ -1 \\ -7.724 \\ -0.55 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \\ -4.4 \\ -1 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ \hline 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \\ -5.77 \\ -0.98 \end{array}$	$\begin{array}{r} -9.26\\ -9.59\\ \hline 0\\ -13.65\\ 1.54e-8\\ 0.06\\ 0.007\\ -8.15\\ 26.84\\ 21654\\ 0.22\\ -4.73\\ -2.5e-4\\ 3.4e+10\\ 0.08\\ 5.4e-5\\ -84095\\ \hline -1\\ -5.47\\ -0.97\\ \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e-82\\ 1e-07\\ 6.9e-19\\ -8.34\\ 1.1e-43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 0\\ 1.1e-26\\ -99999\\ -1\\ -7.67\\ -1\\ \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 - -1.14383 1 0 0 - -1.14383 1 0 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 - -1.14383 -1.14383 - -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.143888 -1.143888 -1.143888 -1.143888 -1.1438	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000
F42 F43 F44 F45 F46 F47 F48 F49 F50 F51 F52 F53 F54 F55 F56 F57 F58 F59 F59	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 5.4e-13\\ 2.03e-15\\ -10e+5\\ -1\\ -7.287\\ -0.98\\ 0.0195\\ \end{array}$	$\begin{array}{c} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ -1 \\ -7.649 \\ -0.974 \\ 0.0021 \end{array}$	$\begin{array}{r} -9.01 \\ \hline -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ 5e - 16 \\ -8.257 \\ 3e - 13 \\ 18935 \\ 0.190 \\ \hline -5.288 \\ -0.06 \\ \hline 1 \\ 5e - 12 \\ 2e - 13 \\ -99987 \\ \hline -1 \\ -5.921 \\ -0.17 \\ 0.0020 \end{array}$	$\begin{array}{r} -7.86\\ -8.55\\ \hline 0\\ -16\\ 3.4e-34\\ 0.0011\\ 4.1e-15\\ -8.341\\ 9.61e-6\\ 127880\\ 0.599\\ -5.11\\ -2.3e-7\\ 4.093\\ 5.5e-17\\ 8.2e-16\\ -92418\\ \hline -1\\ -7.38\\ -0.97\\ 0.00190\end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ -10e + 5 \\ \hline -1 \\ -7.724 \\ -0.55 \\ 0.00190 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \\ -4.4 \\ -1 \\ 0.006 \\ \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ \hline 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \\ -5.77 \\ -0.98 \\ 0.002 \\ \end{array}$	$\begin{array}{r} -9.26\\ -9.59\\ \hline 0\\ -13.65\\ 1.54e-8\\ 0.06\\ 0.007\\ -8.15\\ 26.84\\ 21654\\ 0.22\\ -4.73\\ -2.5e-4\\ 3.4e+10\\ 0.08\\ 5.4e-5\\ -84095\\ \hline -1\\ -5.47\\ -0.97\\ \hline 0.002 \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e - 82\\ 1e - 07\\ 6.9e - 19\\ -8.34\\ 1.1e - 43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 0\\ 1.1e - 26\\ -99999\\ -1\\ -7.67\\ -1\\ 0.002\\ \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 -1.14383 1 0 -1.14383 1 0 -1.14383 1 0 -1.14383 1 0 -1.14383 1 0 -1.14383 1 0 -1.14383 1 0 -1.14383 1 0 -1.14383 1 0 -1.143838 -1.143838 -1.143838 -1.143838 -1.143838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.14388888 -1.14388888888888888888888888888888888888	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 3000
$\begin{array}{c} {\rm F42} \\ {\rm F43} \\ {\rm F44} \\ {\rm F45} \\ {\rm F46} \\ {\rm F47} \\ {\rm F48} \\ {\rm F49} \\ {\rm F50} \\ {\rm F51} \\ {\rm F52} \\ {\rm F53} \\ {\rm F55} \\ {\rm F56} \\ {\rm F57} \\ {\rm F58} \\ {\rm F59} \\ {\rm F60} \end{array}$	$\begin{array}{r} -9.15 \\ \hline 0 \\ -16 \\ 2.76e - 39 \\ 7.15e - 6 \\ 4.38e - 15 \\ -7.191 \\ 6.53e - 12 \\ 270736 \\ 0.195 \\ \hline -5.288 \\ -0.03 \\ \hline 1 \\ 5.4e - 13 \\ 2.03e - 15 \\ \hline -10e + 5 \\ \hline -1 \\ -7.287 \\ -0.98 \\ 0.0195 \\ \hline 1.23e - 32 \end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ -1 \\ -7.649 \\ -0.974 \\ 0.0021 \\ 2.56e - 30 \end{array}$	$\begin{array}{r} -9.01 \\ \hline -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ \hline 0.003 \\ \hline 5e - 16 \\ -8.257 \\ \hline 3e - 13 \\ 18935 \\ \hline 0.190 \\ \hline -5.288 \\ -0.06 \\ \hline 1 \\ \hline 5e - 12 \\ 2e - 13 \\ -99987 \\ \hline -1 \\ -5.921 \\ -0.17 \\ -0.020 \\ \hline 1.28e - 32 \end{array}$	$\begin{array}{r} -7.86 \\ -8.55 \\ \hline 0 \\ -16 \\ 3.4e - 34 \\ 0.0011 \\ 4.1e - 15 \\ -8.341 \\ 9.61e - 6 \\ 127880 \\ 0.599 \\ -5.11 \\ -2.3e - 7 \\ 4.093 \\ 5.5e - 17 \\ 8.2e - 16 \\ -92418 \\ -1 \\ -7.38 \\ -0.97 \\ 0.00190 \\ 1.23e - 32 \end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ -10e + 5 \\ \hline -1 \\ -7.724 \\ -0.55 \\ 0.00190 \\ 1.23e - 32 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \\ -4.4 \\ -1 \\ 0.006 \\ 1.23e - 32 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ \hline 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \\ -5.77 \\ -0.98 \\ 0.002 \\ 4e - 24 \end{array}$	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \\ 21654 \\ 0.22 \\ -4.73 \\ -2.5e - 4 \\ 3.4e + 10 \\ 0.08 \\ 5.4e - 5 \\ -84095 \\ \hline -1 \\ -5.47 \\ -0.97 \\ \hline 0.002 \\ 1.76e - 6 \end{array}$	$\begin{array}{r} -9.47 \\ -10.52 \\ 0 \\ -16 \\ 1.1e - 82 \\ 1e - 07 \\ 6.9e - 19 \\ -8.34 \\ 1.1e - 43 \\ -1053 \\ 0.10 \\ -5.28 \\ -0.63 \\ 1 \\ 0 \\ 1.1e - 26 \\ -99999 \\ -1 \\ 0 \\ 1.1e - 26 \\ -99999 \\ -1 \\ -7.67 \\ -1 \\ 0.002 \\ 1.23e - 32 \end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.14383 1 0 0 -1.143838 -1.143838 -1.143838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.1438838 -1.14388388 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.1438888 -1.14388888 -1.14388888888888888888888888888888888888	100 100 1000 1000 3000 1000
$\begin{array}{c} {\rm F42} \\ {\rm F43} \\ {\rm F44} \\ {\rm F45} \\ {\rm F46} \\ {\rm F47} \\ {\rm F48} \\ {\rm F49} \\ {\rm F50} \\ {\rm F51} \\ {\rm F52} \\ {\rm F53} \\ {\rm F54} \\ {\rm F55} \\ {\rm F56} \\ {\rm F57} \\ {\rm F58} \\ {\rm F59} \\ {\rm F60} \\ {\rm F61} \end{array}$	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 5.4e-13\\ 2.03e-15\\ -10e+5\\ \hline -1\\ -7.287\\ -0.98\\ 0.0195\\ \hline 1.23e-32\\ -1.288\\ \end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ -1 \\ -7.649 \\ -0.974 \\ 0.0021 \\ 2.56e - 30 \\ -1.279 \end{array}$	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ \overline{5e-16} \\ -8.257 \\ \overline{3e-13} \\ 18935 \\ 0.190 \\ -5.288 \\ -0.06 \\ \hline 1 \\ \overline{5e-12} \\ 2e-13 \\ -99987 \\ \hline -1 \\ -5.921 \\ -0.17 \\ 0.0020 \\ \hline 1.28e-32 \\ -1.282 \\ \end{array}$	$\begin{array}{r} -7.86\\ -8.55\\ \hline 0\\ -16\\ \hline 3.4e-34\\ 0.0011\\ \hline 4.1e-15\\ -8.341\\ \hline 9.61e-6\\ 127880\\ \hline 0.599\\ -5.11\\ -2.3e-7\\ \hline 4.093\\ \hline 5.5e-17\\ \hline 8.2e-16\\ -92418\\ \hline -1\\ -7.38\\ \hline -0.97\\ \hline 0.00190\\ \hline 1.28e-32\\ -1.286\end{array}$	$\begin{array}{r} -8.91 \\ -9.60 \\ \hline 0 \\ -13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ -4.07 \\ -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ -10e + 5 \\ \hline -1 \\ -7.724 \\ -0.55 \\ 0.00190 \\ \hline 1.23e - 32 \\ -1.295 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \\ -4.4 \\ -1 \\ 0.006 \\ 1.23e - 32 \\ -1.22 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ \hline 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \\ -5.77 \\ -0.98 \\ 0.002 \\ 4e - 24 \\ -1.296 \end{array}$	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \\ 21654 \\ 0.22 \\ -4.73 \\ -2.5e - 4 \\ 3.4e + 10 \\ 0.08 \\ 5.4e - 5 \\ -84095 \\ \hline -1 \\ -5.47 \\ -0.97 \\ \hline 0.002 \\ 1.76e - 6 \\ -1.261 \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e - 82\\ 1e - 07\\ 6.9e - 19\\ -8.34\\ 1.1e - 43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 1e - 26\\ -99999\\ -1\\ 1.1e - 26\\ -999999\\ -1\\ -7.67\\ -1\\ 0.002\\ 1.23e - 32\\ -1.296\end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 -1.14383 1 0 -1.14383 1 0 -1 -9.660152 -1 0.00004 0 0 1.29695	100 100 1000 1000 3000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 300 1000 200
$\begin{array}{c} {\rm F42} \\ {\rm F43} \\ {\rm F44} \\ {\rm F45} \\ {\rm F46} \\ {\rm F47} \\ {\rm F48} \\ {\rm F49} \\ {\rm F50} \\ {\rm F51} \\ {\rm F52} \\ {\rm F53} \\ {\rm F54} \\ {\rm F55} \\ {\rm F56} \\ {\rm F57} \\ {\rm F58} \\ {\rm F59} \\ {\rm F60} \\ {\rm F61} \\ {\rm F62} \end{array}$	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 5.4e-13\\ 2.03e-15\\ -10e+5\\ -1\\ -7.287\\ -0.98\\ 0.0195\\ 1.23e-32\\ -1.288\\ -45.77\end{array}$	$\begin{array}{c} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ \hline -1 \\ -7.649 \\ -0.974 \\ 0.0021 \\ 2.56e - 30 \\ -1.279 \\ -45.55 \\ \end{array}$	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ \hline 5e-16 \\ -8.257 \\ 3e-13 \\ 18935 \\ 0.190 \\ -5.288 \\ -0.06 \\ \hline 1 \\ 5e-12 \\ 2e-13 \\ -99987 \\ \hline -1 \\ -5.921 \\ -0.17 \\ 0.0020 \\ \hline 1.23e-32 \\ -1.282 \\ -45.77 \end{array}$	$\begin{array}{r} -7.86\\ -8.55\\ \hline 0\\ -16\\ 3.4e-34\\ 0.0011\\ 4.1e-15\\ -8.341\\ 9.61e-6\\ 127880\\ 0.599\\ -5.11\\ -2.3e-7\\ 4.093\\ 5.5e-17\\ 8.2e-16\\ -92418\\ \hline -1\\ -7.38\\ -0.97\\ 0.00190\\ 1.23e-32\\ -1.286\\ -45.77\end{array}$	$\begin{array}{r} -8.91 \\ -8.91 \\ \hline -9.60 \\ \hline 0 \\ -13.55 \\ \hline 5.21e - 5 \\ 0.0010 \\ \hline 2.54e - 16 \\ \hline -8.341 \\ \hline 3.79e - 6 \\ \hline 5951 \\ 0.199 \\ \hline -4.07 \\ \hline -0.085 \\ \hline 1 \\ \hline 2.96e - 7 \\ \hline 8.72e - 9 \\ \hline -10e + 5 \\ \hline -1 \\ \hline -7.724 \\ \hline -0.55 \\ \hline 0.00190 \\ \hline 1.23e - 32 \\ \hline -1.295 \\ \hline -45.77 \\ \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \\ -4.4 \\ -1 \\ 0.006 \\ 1.23e - 32 \\ -1.22 \\ -45.77 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \\ -5.77 \\ -0.98 \\ 0.002 \\ 4e - 24 \\ -1.296 \\ -45.77 \end{array}$	$\begin{array}{r} -9.26\\ -9.59\\ \hline 0\\ -13.65\\ 1.54e-8\\ 0.06\\ 0.007\\ -8.15\\ 26.84\\ 21654\\ 0.22\\ -4.73\\ -2.5e-4\\ 3.4e+10\\ 0.08\\ \hline 5.4e-5\\ -84095\\ \hline -1\\ -5.47\\ -0.97\\ \hline 0.002\\ 1.76e-6\\ -1.261\\ -45.31\end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e-82\\ 1e-07\\ 6.9e-19\\ -8.34\\ 1.1e-43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 0\\ 1.1e-26\\ -99999\\ -1\\ -7.67\\ -1\\ 0.002\\ 1.23e-32\\ -1.296\\ -45.77\end{array}$	$\begin{array}{c} -10 \\ -10 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$	100 100 1000 1000 3000 1000 2000 1000
$\begin{array}{c} {\rm F42} \\ {\rm F43} \\ {\rm F44} \\ {\rm F45} \\ {\rm F46} \\ {\rm F47} \\ {\rm F48} \\ {\rm F49} \\ {\rm F50} \\ {\rm F51} \\ {\rm F52} \\ {\rm F53} \\ {\rm F55} \\ {\rm F56} \\ {\rm F57} \\ {\rm F58} \\ {\rm F59} \\ {\rm F60} \\ {\rm F61} \\ {\rm F62} \\ {\rm F63} \end{array}$	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 5.4e-13\\ 2.03e-15\\ -10e+5\\ \hline -1\\ -7.287\\ -0.98\\ 0.0195\\ \hline 1.23e-32\\ -1.288\\ -45.77\\ 0.181\\ \end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ \hline -1 \\ -7.649 \\ -0.974 \\ 0.0021 \\ 2.56e - 30 \\ -1.279 \\ -45.55 \\ 0.11 \\ \end{array}$	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ \overline{5e-16} \\ -8.257 \\ \overline{3e-13} \\ 18935 \\ 0.190 \\ -5.288 \\ -0.06 \\ \hline 1 \\ \overline{5e-12} \\ 2e-13 \\ -99987 \\ -1 \\ -5.921 \\ -0.17 \\ 0.0020 \\ \hline 1.28e \\ -32 \\ -45.77 \\ \overline{1.4e-17} \end{array}$	$\begin{array}{r} -7.86\\ -8.55\\ \hline 0\\ -16\\ 3.4e-34\\ 0.0011\\ 4.1e-15\\ -8.341\\ 9.61e-6\\ 127880\\ 0.599\\ -5.11\\ -2.3e-7\\ 4.093\\ 5.5e-17\\ 8.2e-16\\ -92418\\ \hline -1\\ -7.38\\ -0.97\\ 0.00190\\ 1.23e-32\\ -1.286\\ -45.77\\ 1.4e-22\end{array}$	$\begin{array}{r} -8.91 \\ -8.91 \\ \hline -9.60 \\ \hline 0 \\ \hline 13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ \hline -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ \hline -4.07 \\ \hline -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ \hline -10e + 5 \\ \hline -1 \\ \hline -7.724 \\ \hline -0.55 \\ 0.00190 \\ \hline 1.23e - 32 \\ \hline -1.295 \\ \hline -45.77 \\ 2.49e - 9 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \\ -4.4 \\ -1 \\ 0.006 \\ 1.23e - 32 \\ -1.22 \\ -45.77 \\ 3.30 \\ \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ -6.90 \\ 33.71 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \\ -5.77 \\ -0.98 \\ 0.002 \\ 4e - 24 \\ -1.296 \\ -45.77 \\ 1.1e - 5 \end{array}$	$\begin{array}{r} -9.26\\ -9.59\\ \hline 0\\ -13.65\\ 1.54e-8\\ 0.06\\ 0.007\\ -8.15\\ 26.84\\ 21654\\ 0.22\\ -4.73\\ -2.5e-4\\ 3.4e+10\\ 0.08\\ 5.4e-5\\ -84095\\ \hline -1\\ -5.47\\ -0.97\\ \hline 0.002\\ 1.76e-6\\ -1.261\\ -45.31\\ 0.2\end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e - 82\\ 1e - 07\\ 6.9e - 19\\ -8.34\\ 1.1e - 43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 1\\ 0\\ 1.1e - 26\\ -99999\\ -1\\ -7.67\\ -1\\ 0.002\\ 1.28e - 32\\ -1.296\\ -45.77\\ 2.1e - 34\end{array}$	$\begin{array}{c} -10 \\ -10 \\ 0 \\ -16 \\ 0 \\ 0 \\ 0 \\ -n+1 \\ 0 \\ -4930 \\ 0 \\ -114383 \\ 1 \\ 0 \\ 0 \\ -1 \\ -9.660152 \\ -1 \\ 0.00004 \\ 0 \\ 1.29695 \\ -45.778 \\ 0 \end{array}$	100 100 1000 1000 3000 1000 200 1000 200 1000 200 1000 200 1000
$\begin{array}{c} {\rm F42} \\ {\rm F43} \\ {\rm F44} \\ {\rm F45} \\ {\rm F46} \\ {\rm F47} \\ {\rm F48} \\ {\rm F49} \\ {\rm F50} \\ {\rm F51} \\ {\rm F52} \\ {\rm F53} \\ {\rm F54} \\ {\rm F55} \\ {\rm F56} \\ {\rm F57} \\ {\rm F58} \\ {\rm F59} \\ {\rm F60} \\ {\rm F61} \\ {\rm F62} \\ {\rm F63} \\ {\rm F64} \end{array}$	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 2.03e-13\\ 2.03e-15\\ -10e+5\\ \hline -1\\ -7.287\\ -0.98\\ 0.0195\\ \hline 1.23e-32\\ -1.288\\ -45.77\\ -0.181\\ -186\end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ \hline -1 \\ -7.649 \\ -0.974 \\ 0.0021 \\ 2.56e - 30 \\ -1.279 \\ -45.55 \\ 0.11 \\ -186 \end{array}$	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ \hline 5e - 16 \\ -8.257 \\ \hline 3e - 13 \\ 18935 \\ 0.190 \\ \hline -5.288 \\ -0.06 \\ \hline 1 \\ 5e - 12 \\ 2e - 13 \\ -99987 \\ \hline -1 \\ -5.921 \\ -0.17 \\ 0.0020 \\ \hline 1.23e - 32 \\ -1.282 \\ \hline -45.77 \\ \hline 1.4e - 17 \\ \hline -86 \\ \end{array}$	$\begin{array}{r} -7.86\\ -8.55\\ \hline 0\\ -16\\ 3.4e-34\\ 0.0011\\ 4.1e-15\\ -8.341\\ 9.61e-6\\ 127880\\ 0.599\\ -5.11\\ -2.3e-7\\ 4.093\\ 5.5e-17\\ 8.2e-16\\ -92418\\ \hline -1\\ -7.38\\ -0.97\\ \hline 0.00190\\ 1.23e-32\\ -1.286\\ -45.77\\ 1.4e-22\\ -186\end{array}$	$\begin{array}{r} -8.91 \\ -8.91 \\ \hline -9.60 \\ \hline 0 \\ \hline 13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ \hline -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ \hline -4.07 \\ \hline -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ \hline -10e + 5 \\ \hline -1 \\ \hline -7.724 \\ \hline -0.55 \\ \hline 0.00190 \\ \hline 1.23e - 32 \\ \hline -1.295 \\ \hline -45.77 \\ 2.49e - 9 \\ \hline -186 \\ \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \\ -4.4 \\ -1 \\ 0.006 \\ 1.23e - 32 \\ -1.22 \\ -45.77 \\ 3.30 \\ -1.85.4 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ 3.8e - 4 \\ 0.1 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \\ -5.77 \\ -0.98 \\ 0.002 \\ 4e - 24 \\ -1.296 \\ 0.45.77 \\ 1.1e - 5 \\ -186.6 \\ \end{array}$	$\begin{array}{r} -9.26\\ -9.59\\ \hline 0\\ -13.65\\ 1.54e-8\\ 0.06\\ 0.007\\ -8.15\\ 26.84\\ 21654\\ 0.22\\ -4.73\\ -2.5e-4\\ 3.4e+10\\ 0.08\\ 5.4e-5\\ -84095\\ \hline -1\\ -5.47\\ -0.97\\ \hline 0.002\\ 1.76e-6\\ -1.261\\ -45.31\\ 0.2\\ -186.5\\ \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -16\\ 1.1e - 82\\ 1e - 07\\ 6.9e - 19\\ -8.34\\ 1.1e - 43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 0\\ 1.1e - 26\\ -99999\\ -1\\ 1.1e - 26\\ -99999\\ -1\\ 1.28e - 32\\ -1.296\\ -45.77\\ 2.1e - 34\\ -186.7\end{array}$	-10 -10 0 -16 0 0 -n+1 0 -4930 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 1 0 0 - -1.14383 -1 -1.000004 0 1.296955 -45.7788 0 -1.866.730	100 100 1000 500 100
$\begin{array}{c} {\rm F42} \\ {\rm F43} \\ {\rm F44} \\ {\rm F45} \\ {\rm F46} \\ {\rm F47} \\ {\rm F48} \\ {\rm F49} \\ {\rm F50} \\ {\rm F51} \\ {\rm F52} \\ {\rm F53} \\ {\rm F54} \\ {\rm F55} \\ {\rm F56} \\ {\rm F57} \\ {\rm F58} \\ {\rm F59} \\ {\rm F60} \\ {\rm F61} \\ {\rm F62} \\ {\rm F63} \\ {\rm F64} \\ {\rm F65} \end{array}$	$\begin{array}{r} -9.15\\ \hline 0\\ -16\\ 2.76e-39\\ 7.15e-6\\ 4.38e-15\\ -7.191\\ 6.53e-12\\ 270736\\ 0.195\\ -5.288\\ -0.03\\ \hline 1\\ 5.4e-13\\ 2.03e-15\\ -10e+5\\ -1\\ -7.287\\ -0.98\\ 0.0195\\ \hline 1.23e-32\\ -1.288\\ -45.77\\ 0.181\\ -186\\ -3.5\end{array}$	$\begin{array}{r} -8.71 \\ \hline 0 \\ -15.81 \\ 1.09e - 18 \\ 1.15 \\ 0.016 \\ -8.333 \\ 14.67 \\ 51291 \\ 0.980 \\ -5.286 \\ -3.2e - 13 \\ 7.07 \\ 0.032 \\ 2.7e - 06 \\ -99620 \\ \hline -1 \\ -7.649 \\ -0.974 \\ 0.0021 \\ 2.56e - 30 \\ -1.279 \\ -45.55 \\ 0.11 \\ -186 \\ -3.5 \end{array}$	$\begin{array}{r} -9.01 \\ -9.90 \\ \hline 0 \\ -12.33 \\ 0.003 \\ 0.003 \\ \overline{5e-16} \\ -8.257 \\ \overline{3e-13} \\ 18935 \\ 0.190 \\ -5.288 \\ -0.06 \\ \hline 1 \\ 5e-12 \\ 2e-13 \\ -99987 \\ -1 \\ -5.921 \\ -0.17 \\ 0.0020 \\ \hline 1.23e-32 \\ -1.282 \\ -45.77 \\ \overline{1.4e-17} \\ -186 \\ -3.5 \end{array}$	$\begin{array}{r} -7.86\\ -8.55\\ \hline 0\\ -16\\ 3.4e-34\\ 0.0011\\ 4.1e-15\\ -8.341\\ 9.61e-6\\ 127880\\ 0.599\\ -5.11\\ -2.3e-7\\ 4.093\\ 5.5e-17\\ 8.2e-16\\ -92418\\ -1\\ -7.38\\ -0.97\\ \hline 0.00190\\ 1.23e-32\\ -1.286\\ -45.77\\ 1.4e-22\\ -186\\ -3.5\\ \end{array}$	$\begin{array}{r} -8.91 \\ -8.91 \\ \hline -9.60 \\ \hline 0 \\ \hline 13.55 \\ 5.21e - 5 \\ 0.0010 \\ 2.54e - 16 \\ \hline -8.341 \\ 3.79e - 6 \\ 5951 \\ 0.199 \\ \hline -4.07 \\ \hline -0.085 \\ \hline 1 \\ 2.96e - 7 \\ 8.72e - 9 \\ \hline -10e + 5 \\ \hline -1 \\ \hline -7.724 \\ \hline -0.55 \\ \hline 0.00190 \\ \hline 1.23e - 32 \\ \hline -1.295 \\ \hline -45.77 \\ \hline 2.49e - 9 \\ \hline -186 \\ \hline -3.5 \end{array}$	$\begin{array}{r} -6.58 \\ -5.73 \\ 3.957 \\ -5.12 \\ 5.1e - 60 \\ 1e - 126 \\ 3.2e - 14 \\ -5.16 \\ 1e - 121 \\ -4930 \\ 0.14 \\ -5.28 \\ -0.74 \\ 1 \\ 0 \\ 0.1 \\ -65299 \\ -1 \\ -4.4 \\ -1 \\ 0.006 \\ 1.23e - 32 \\ -1.22 \\ -45.77 \\ 3.30 \\ -185.4 \\ -3.5 \end{array}$	$\begin{array}{r} -8.43 \\ -7.41 \\ 0 \\ -16 \\ 1.1e - 12 \\ 3.8e - 4 \\ 0.1 \\ 3.8e - 4 \\ 0.1 \\ 15485 \\ 0.48 \\ -5.28 \\ -0.001 \\ 5e + 11 \\ 2e - 5 \\ 3e - 8 \\ -99999 \\ -1 \\ -5.77 \\ -0.98 \\ 0.002 \\ 4e - 24 \\ -1.296 \\ -45.77 \\ 1.1e - 5 \\ -186.6 \\ -2.951 \end{array}$	$\begin{array}{r} -9.26 \\ -9.59 \\ \hline 0 \\ -13.65 \\ 1.54e - 8 \\ 0.06 \\ 0.007 \\ -8.15 \\ 26.84 \\ 21654 \\ 0.22 \\ -4.73 \\ -2.5e - 4 \\ 3.4e + 10 \\ 0.08 \\ 5.4e - 5 \\ -84095 \\ \hline -1 \\ -5.47 \\ -0.97 \\ \hline 0.002 \\ 1.76e - 6 \\ -1.261 \\ -45.31 \\ 0.2 \\ -186.5 \\ -2.42 \end{array}$	$\begin{array}{r} -9.47\\ -10.52\\ 0\\ -10.52\\ 0\\ 1.1e-82\\ 1e-07\\ 6.9e-19\\ -8.34\\ 1.1e-43\\ -1053\\ 0.10\\ -5.28\\ -0.63\\ 1\\ 0\\ -5.28\\ -0.63\\ 1\\ 0\\ 1.1e-26\\ -99999\\ -1\\ 1.28e-32\\ -1.296\\ -45.77\\ 2.1e-34\\ -186.7\\ -3.5\\ \end{array}$	$\begin{array}{c} -10 \\ -10 \\ 0 \\ -16 \\ 0 \\ 0 \\ 0 \\ 0 \\ -n+1 \\ 0 \\ 0 \\ -4930 \\ 0 \\ -114383 \\ 1 \\ 0 \\ 0 \\ -114383 \\ 1 \\ 0 \\ 0 \\ -11660152 \\ -1 \\ 0.00004 \\ 0 \\ 1.29695 \\ -45.778 \\ 0 \\ -186.730 \\ -3.5 \\ \end{array}$	$\begin{array}{c} 100\\ 100\\ 1000\\ 500\\ 100\\ 5000\\ 1000\\ 500$

*Notation e - a means 10^{-a} .

	CEP	FEP	LEP	EEP	RLEP	WMCEP		CMA-ES	IIW-PSO	GA-JG	WMCEP
CEP	0	-2.23	-1.03	$^{-1}$	0.57	0.59	IIW-PSO	0	-76	-5.2	547e - 8
FEP	2.23	0	1.19	1.23	2.81	2.82	GA-IG	76	0	71.6	71
\mathbf{LEP}	1.03	-1.19	0	0.033	1.61	1.63	CMA-ES	5.2	-71.6	0	5.2
\mathbf{EEP}	1	-1.23	-0.033	0	1.58	1.59	WMCEP	$-547\mathrm{e}-8$	-71	-5.2	0
RLEP	-0.57	-2.81	-1.61	-1.58	0	0.016					
WMCEP	-0.59	-2.82	-1.63	-1.59	-0.016	0					

TABLE 4. Contrast estimation method results. Estimators highlight WM-CEP as the best performing algorithm.

Therefore, the required time for CMA-ES to evaluate each iteration is 2.26 times more than that of WMCEP. This difference is very crucial in real world applications where cost functions require many iterations in order to reach the global minimum.

6.2. Variable bounds. Some applications force bounds on their parameters or coefficients, which must be adapted. As EAs search the map with a population, it is possible that some variables of individuals are produced out of frontiers. In order to fix this problem, two decisions have usually been made. In the first one, the variable set to the frontier value when it comes out. In the second decision, the variable set to the uniform random number inside the searching map. The first decision for fixing this problem makes the CMA-ES lose its destination (Figure 11). The second decision results in oscillation in the algorithm output (Figure 10). It can be seen that the proposed method is not sensitive to boundary limits, because by the normalized coefficient in Equation (8), the algorithm prevents from producing offsprings out of boundaries.

6.3. Variable numbers. Table 6 compares performances of CMA-ES and WMCEP in a higher number of variables on five functions while bound limitation is forced on both algorithms. In part IV, bounds were not imposed on CMA-ES when the global minimum was inside the searching map and there was no other better minimum outside the bounds. However, in some cost functions like f25, there are deeper minimums out of bounds, so the algorithm is forced to search inside the searching map. Thus, oscillation in results of some algorithms (like CMA-ES) in Table 3 is due to this decision. It can be seen in Table 5 that the CMA-ES is sensitive to number of variables, but WMCEP is not.



FIGURE 10. Setting the value of variable to the frontier value



FIGURE 11. Set uniform random value to the variable

TABLE 5. Test sensitivity of CMA-ES and WMCEP against forcing bound limitations for variables

	Dimension	Generation	CMA-ES	WMCEP	Dimension	Generation	CMA-ES	WMCEP	Global minimum
F 1	40	400	863	01.28	10	100	_02.64	92.64	02.65
	40	400	000	-31.20	10	100	-52.04	-52.04	- 32.00
F2	40	1000	276.32	276.32	10	100	276.32	276.32	276.32
F3	40	1000	2425	153	10	500	25.08	23.29	20.91
$\mathbf{F4}$	40	1000	62.20	151	10	500	30.85	29.77	20.91
F5	40	100	564	51.53	10	50	62.52	51.53	51.53

6.4. **Population size.** Table 6 compares the two algorithms CMA-ES and WMCEP with a certain population. Five functions were selected for this comparison. Tournament size (q) in WMCEP is proportional to the population and is calculated by the equation $q = \frac{10 \times \text{population}}{100}$.

TABLE 6. Test sensitivity of population size for CMA-ES and WMCEP

Function	Population	Generation	WMCEP	CMA-ES	Global minimum
F1	20	500	-92.65	-92.65	-92.65
	50	200	-92.65	-92.65	-92.65
	100	100	-92.65	-92.65	-92.65
	200	50	-92.62	-92.64	-92.65
F2	20	500	276.32	276.32	276.32
	50	200	276.32	276.32	276.32
	100	100	276.32	276.32	276.32
	200	50	297.62	276.55	276.32
F3	20	1500	22.89	25.88	20.91
	50	600	24.193	26.282	20.91
	100	300	25.08	23.29	20.91
	200	150	20.97	21.90	20.91
F4	20	2500	40.11	34.59	20.91
	50	1000	30.85	31.25	20.91
	100	500	29.77	30.85	20.91
	200	250	25.93	26.87	20.91
F5	20	250	51.53	51.53	51.53
	50	100	51.53	51.53	51.53
	100	50	51.53	51.53	51.53
	200	25	51.53	51.53	51.53

In this part, the number of recalling cost functions for all different populations is consistent. As can be seen, both algorithms were slightly sensitive to population size. It is predictable that increasing the number of individuals in each generation gives them more information about better and worse places for breeding. Therefore, WMP will be more accurate in estimating the global minimum.

7. Application. The MVC (Minimum Variance Controller), also referred to as optimal H2 control and first derived in [24] by Astrom (1970) and Box and Jenkins (1970) [25], is the best possible feedback control for linear systems in the sense that it achieves the smallest possible closed-loop output variance [26]. When the model of the process are known, or can be identified, MV controller can be designed to minimize the variance of output. Although almost all real-world systems are nonlinear in behavior, most of the introduced methods for estimating minimum variance use linear approaches and require linear models [27]. MV controllers can be enhanced to deal with nonlinear systems if nonlinear models are considered. However, designing nonlinear MVC especially using Neural Network (NN-MVC) has some drawbacks:

1) In order to design MVC, the explicit relations between outputs and inputs must be executable. This relation is defined implicitly in the nonlinear models [28,29]. Suppose that the plant can be described by the following model,

$$y(t+1) = f(y(t), y(t-1), \dots, y(t-n_y), u(t), u(t-1), \dots, y(t-n_u))$$
(9)

where f(.) is a neural network, in which y_t and u_t denote the output and the input signal vectors respectively. Inverse models of systems are necessary for designing MVC. The input-output relation of the neural network modeling the plant inverse is:

$$u(t) = f^{-1}(y(t+1), y(t), y(t-1), \dots, y(t-n_y), u(t-1), \dots, y(t-n_u))$$
(10)

Obtaining inverse of neural network has some difficulties such as: **a**) The actual operational inputs may be hard to define a priori; **b**) If a nonlinear system is not one-one, then an incorrect inverse can be obtained; Finding inverse of nonlinear neural network is a tedious task (if possible), and **c**) Control signal is not in hand before obtaining inverse function, and the inverse function is not executable before having control signal (unless function f(.) is known or can be estimated).

These problems cause that researchers define approximated form of neural networks for NN-MVC designing. Some researchers have suggested the affine model of neural networks in which the relation between input and output can be defined explicitly as follows [28]:

$$y(t+1) = f(X(t)) + g(X(t))u(t) + e(t)$$
(11)

where e(t) is model mismatch and

$$X(t) = [y(t), y(t-1), \dots, y(t-n_y), u(t), u(t-1), \dots, y(t-n_u)]$$

In addition, the linear approximation has been used in literature such as bilinear approximation of Equation (9) that may be parameterized as [29]:

$$y(t+1) = Ay(t) + Bu(t) + g(.)$$
(12)

where an assumption is made that B is non-zero. A and B are unknown diagonal parameter matrices and g(.) is the nonlinear part of the equivalent model.

These models are not accurate and are not universal models. These methods can be used in designing many kinds of controllers, but considering that the MVC is an optimal controller that must be accurate in reaching minimum variance, it can be a big disadvantage for these approximated methods. Even, these methods can be less accurate than linear MV methods. 2) Another drawback of using neural network is training issue. Training neural networks is a high dimensional-multimodal optimization task and weight space can be extremely rugged and has many local minima. This problem is avoiding using full neural network model directly as a controller.

The strategy of this paper is to use evolutionary algorithms for weight optimization in domains where gradient methods cannot be directly applied, or where gradient methods are less effective than in simple supervised learning applications.

In this paper, for the first time, EA has been used for designing MVC by training full neural network model. Based on authors' information, the proposed method is a new idea and has not been proposed in previous published literatures. In this regard, WMCEP is used for optimizing the neural network weights. Obviously, a search method that cannot escape from local minima will have difficulty in finding an optimal solution. This method can fill up the gap between advantages of NN-MVC and difficulty in obtaining $f^{\Box 1}(.)$.

Consider the neural model for the controller is represented by a two-layer artificial neural network. The neural networks are then trained by WMCEP for a proper number of iterations. After training is completed, the controller is applied on loop, and the output variance is calculated for each individual and all the neural networks are ranked based on the values of their fitness indexes. Figure 12 shows the flowchart of the mentioned WMCEP procedure when the NN-MVC design is adopted.

```
Creation of the initial population with proper individual dimension

Generate initial network

While not Stop Criterion do

For (for all individuals)

Set up corresponded NN-MVC by weight values defined in the individual

Sample output of loop on control of NN-MVC

Evaluate the cost (variance of sampled data)

End for

Set up compete among individuals and decide the winners

Calculate mean point of winner individuals

Reproduce new individuals using the winner of the previous generation

and information of mean point

Consider new individuals as the new weights of NN.

End while
```

FIGURE 12. Pseudo-code for NN-MVC design by MCEP

A block scheme of the heuristic neural network process model is shown in Figure 13.



FIGURE 13. The process modelling block scheme using heuristic NN-MVC

7.1. Simulation result. The study example is a CSTR (Continuous Stirred-Tank Reactor) with a first-order exothermic reaction provided in [30]. It is a typical chemical engineering process which is intensively studied at the control and system identification

areas. The dynamic behavior for this CSTR (Figure 14) can be described using the following nondimensional normalized equations:

$$\dot{x}_1 = -x_1 + D_a(1-x_1)e^{\frac{x_2}{1+x_2/\lambda}} \quad \dot{x}_2 = -x_2 + BD_a(1-x_1)e^{\frac{x_2}{1+x_2/\lambda}} - \beta(x_2-x_c)$$
(13)

where x_1 and x_2 are the reactor dimensionless concentration and temperature respectively. The case study under consideration is a regulation of outlet reactant concentration x_1 . Coolant temperatures x_c is the manipulated variable. One set of parameter values B = 1.0, $\beta = 0.3$, $\lambda = 20.0$ and $D_a = 0.072$ which yields an open-loop system with a single stable steady state for all fixed values of the input is selected in [0 23] ([31]). The detailed nomenclature for this exothermic CSTR can be found in [32].



FIGURE 14. Cross-sectional diagram of continuous stirred-tank reactor

The input range real value range is [0 23]. The output is bounded at range [0 1] for introduced input range [31]. The starting situation is a stable steady situation with the initial states $x_1 = 0.6219$ and $x_2 = 3.7092$ and input $u_t = 14$.

The output Yt with an additive linear disturbance is

$$Yt = (x_1)t + Dt \tag{14}$$

where Dt is an additive disturbance. The disturbance model is an AR (AutoRegressive) model defined as:

$$Dt = \frac{e_t}{1 - 0.95q^{-1}} \tag{15}$$

where e_t is a Gaussian white noise with zero mean and variance 0.001.

NN-MVC has been designed using the WMCEP method for reducing output variance of the benchmark system. Population size for WMCEP is equal to 100; and it is repeated 20 times for reducing the effect of the chance and increasing the reliability in the results. The best results among 20 ones are included in this paper. They are run until the prespecified generation (100) is reached. The initial population is generated randomly with variance 3. The weight values (genes) are bounded in range $[-10\ 10]$. Fitness is given by cost function J for each individual of the population, where J is the variance of output as shown in Equation (16), where the summation is performed on overall output samples y and y_d is the desired or target value of output for a given input vector.

$$J = \sigma_y^2 = \frac{1}{N-1} \sum_{k=1}^N (y(k) - \bar{y} - y_d)^2, \quad \bar{y} = \frac{1}{N} \sum_{k=1}^N y(k)$$
(16)

The introduced algorithms are used to evolve the weights of the feedforward neural network with two layered structures. The input layer has eight nodes; the hidden layer has 10 hidden nodes; the output layer has *one* output nodes. Hidden transfer function is sigmoid function, and the output transfer function is a linear activation function.

Figure 15 shows the cost curve corresponding to the best cost value found in the last generation. This figure shows that the WMCEP can find the acceptable network weights in a shorter number of iterations. It admits the capability of this method in fast training the neural network MVC. The minimum variance (minimum cost) found by this the proposed algorithm is 9.37×10^{-5} .



FIGURE 15. Cost values via iteration

Figure 16 shows disturbance, control signal and output data of the NN-MV designed controller by WMCEP. Optimized weights values found by WMCEP are included in Appendix A.

The optimality of the designed controller by WMCEP can be analyzed using a toolbox. The multivariate controller performance assessment toolbox was developed by the Computer Process Control Group at the University of Alberta to allow performance assessment of linear controller using the Filtering and Correlation (FCOR) Algorithm [33]. The control performance index is a single scalar usually scaled to lie within [0, 1], where values close to 0 indicate poor performance, and values close to 1 mean better/tighter control. This indeed holds when perfect control is considered as a benchmark. Here, the performance of the designed NN-MVC will be assessed by the performance assessment toolbox. The CSTR is linearized around the operating point. Then the linear model and output data of NN-MVC is applied to the performance assessment toolbox. Figure 17 shows the result of assessing the designed controller. It shows that the minimum variance index of the designed controller is 1.0281, which is higher than one, so the controller is better than optimal *linear* MV controller is. Moreover, this result can be admitted by the approach used in [32] for this system in the similar situation, in which linear method reaches the variance 3.51×10^{-3} , which is higher than that of the proposed method. In other words, the designed nonlinear controller has been reached to the minimum variance is lower than that of the optimal linear methods.



FIGURE 16. Realizations of disturbance, NN-MVC control signal and output data



FIGURE 17. Realizations of disturbance, NN-MVC control signal and output data

8. Conclusions. In this paper, a developed version of CEP was proposed. There was an attempt to use the location and cost information of each parent for determining the best area for breeding the offspring. It was tried to steer the offspring toward the best parents' areas and they were prevented from getting close to worst parents using the state feedback controller. Two groups of algorithms from in and out of the EP family were selected for comparison. WMCEP had noticeable results against other EP variants. It had the best results for almost all cost functions (about 90 percent of the cost functions) in comparison with CEP, LEP, EEP, RLEP and FEP. It also demonstrated acceptable results outside the EP frontier. The proposed method was compared with eight well-known algorithms. Only CMA-ES had comparable results with WMCEP. However, CMA-ES needed heavy computation and higher CPU time for evaluating each generation. It also had problems with bounds of the variables that were not seen in the WMCEP performance. Many cost functions were selected from several references, which all of them are well-known functions in the optimization field. The proposed method is used in designing the nonlinear minimum variance controller for CSTR (Continuous Stirred-Tank Reactor) benchmark system. The designed nonlinear controller has been reached to minimum variance which is lower than that of existing methods. The future prospect of the approach proposed here is to study the accuracy of the WMCEP for obtaining better results and test it on real-world applications.

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Appendix A.

Wij	j = 1	j=2	j = 3	j=4	j = 5	j = 6	j = 7	j = 8	j=9	j = 10
i = 1	-2.7763	-6.1925	-1.9250	3.8635	-9.1758	6.4905	-1.2005	1.4717	-8.5236	-5.9282
i=2	-9.4702	-3.9335	3.8145	9.3231	-9.1604	-8.2248	3.2686	2.4480	-3.8139	7.6736
i = 3	-2.3129	3.4643	-4.2889	-7.7741	9.0812	9.7962	10.441	-3.6376	-2.9007	3.3854
i = 4	-8.8890	1.6644	-1.9433	-1.3899	-5.0392	-7.2601	0.4129	-2.6124	-2.4283	-0.7510
i = 5	-2.8017	8.3229	-2.0793	4.4994	-4.6531	-5.2277	-6.6811	1.9210	1.9698	10.059
i = 6	8.8527	5.9410	2.1878	8.4467	0.6824	0.7140	-5.3913	6.1774	1.6181	-10.700
i = 7	3.5483	9.7259	0.0255	0.0473	3.5124	-9.5840	-7.6692	7.0161	5.6355	8.9759
i = 8	-3.8701	6.6945	5.9696	6.2335	-1.9470	2.2898	7.3698	1.8640	-9.8845	-5.5877
W_{1j}	j = 1	j=2	j = 3	j=4	j = 5	j=6	j = 7	j = 8	j=9	j = 10
o = 1	-6.0359	4.6606	-9.6462	0.0184	3.5209	0.5573	-7.1110	-8.0571	-6.6251	-3.7482
b_j	j = 1	j=2	j=3	j=4	j = 5	j = 6	j=7	j = 8	j=9	j = 10
	8.6359	1.5325	-7.5322	3.5676	-2.8395	5.1268	-4.1412	1.5594	9.1530	4.3419
b ₁₁	9.1845									

TABLE 7. Optimized weights values found by WMCEP

where w_{ij} is the connection weight from the *i*th node of input layer to the *j*th node of hidden layer, b_j is the threshold of the *j*th hidden layer input, w_{1j} is the connection weight from the *j*th hidden node to the output node, and b_{11} is the threshold of the output unit.